

## A SILENT CHAIN FOR RESTRAINING CHORDAL ACTION

### REFERENCE TO RELATED APPLICATIONS

This application claims priority from Japanese Application No. 2002-354698, filed December 26, 2002, under the benefit of 35 USC §119 (a)-(d) or § 365(b). The  
5      aforementioned application is hereby incorporated by reference.

### BACKGROUND OF THE INVENTION

#### FIELD OF THE INVENTION

The present invention pertains to the field of silent chains. More particularly, an improvement in structure to restrain chordal oscillation of a chain span of a silent chain  
10      and to improve noise and oscillation performance.

### DESCRIPTION OF RELATED ART

Silent chains have been used as a power transmission chain in automobiles, motorcycles and the like. A silent chain is generally comprised of a plurality of link plates each having a pair of teeth and pin apertures, arranged in lateral and longitudinal  
15      directions, and pivotably connected by connecting pins inserted in the pin apertures. Each of the teeth are formed of an inside flank and an outside flank. During operation of a silent chain, power is transmitted from a drive sprocket to a driven sprocket through the engagement of the inside flank and/or the outside flank with a sprocket tooth.

Chordal action, or oscillation of a chain span, occurs at the time of engagement of  
20      the chain with a sprocket, in this case the silent chain wraps around the chain polygonally. In order to prevent such a chordal action and to reduce noise, as shown in Japanese patent application laying-open publication No. 8-74940, the same inventor as the present invention, proposed a silent chain where a radius of curvature  $R$  of an inside flank of a link plate is made more than generally double the length of a chain pitch  $P$ , so that the link  
25      plate is raised through the inside flank at the time of engagement with a sprocket tooth.

The above prior art application is directed to lifting up a chain span to a position in the vicinity of a vertex of polygonal shaped movements of the chain around the sprocket. However, it has been found that in the actual product, a lift-up of a chain span becomes insufficient at times due to errors in manufacture and assembly and as a result, a chordal action cannot be perfectly removed.

## SUMMARY OF THE INVENTION

The present invention is directed to a silent chain where a plurality of link plates each having a pair of teeth and pin apertures are interlaced in link thickness and length directions and pivotably connected by connecting pins inserted in the pin apertures. Each of the teeth are formed of an inside flank and an outside flank. An inside flank of one link plate projects from an outside flank of another link plate whose tooth overlaps a tooth of one link when a chain is pulled straight. The inside flank and the outside flank are formed in such a way that  $0.021 \cdot P \leq \delta_{\max} \leq 0.063 \cdot p$  is satisfied where  $P$  is a chain pitch and  $\delta_{\max}$  is a maximum projection of the inside flank relative to the outside flank.

At the time of engagement with a sprocket, an inside flank of the link plate contacts and interferes with a sprocket tooth and the chain span is lifted up. At this time, since the maximum projection of the inside flank satisfy the above-mentioned inequality, interference of the inside flank with the chain is determined at an appropriate value. Therefore, when the silent chain engages with the sprocket, the chain is lifted up at least to a position that is a vertex of polygonal shaped movements of the chain around the sprocket. The position is located at a position further up than the range of chordal movements of the silent chain that engages the sprocket teeth only at the outside flanks of link plates. Thereby, at the time of engagement with a sprocket, the chain span may be lifted up to a position that is hard to be influenced by a chordal action of a chain span. As a result, a chordal action can be securely restrained and noise and oscillation performance can be advanced.

Preferably, the inside flank and the outside flank are formed in such a way that  $0.035 \cdot P \leq \delta_{\max} \leq 0.063 \cdot p$  is satisfied. In this case, at the time of engagement with a sprocket, a chain span may be lifted up to a position that is very hard to be influenced by a chordal action of a chain span. As a result, a chordal action can be further securely

refrained and noise and oscillation performance can be further advanced. Preferably, the outside flank is formed of a flat surface and the inside flank is formed of a circular arc surface.

According to another aspect of the present invention, the link plates of the chain are comprised of a first link plate having a first maximum projection  $\delta_1\text{max}$  and a second link plate having a second maximum projection  $\delta_2\text{max}$  that is different from  $\delta_1\text{max}$ . The first and second link plates are disposed in a random pattern along the length of a chain. In this case, at the time of engagement with a sprocket, a first lift-up of a chain span by the first link plate differs from a second lift-up of a chain span by the second link plate, and the first and second lift-up is repeated aperiodically. Thereby, when the chain engages with the sprocket at an upper position that is not affected by chordal action of a chain span, periodical chordal oscillation of a chain span can be restrained and thus, noise and oscillation performance can be further improved as compared to the engagement where constant lift-up is periodically repeated.

According to still another aspect of the present invention, the silent chain is a random chain where link plates are formed of a first link plate having a first chain pitch  $P_1$  and a second link plate having a second chain pitch  $P_2$  that is different from  $P_1$ , and the first and second link plates are disposed at a random pattern along the length of a chain. In this case, at the time of engagement with a sprocket, a first engagement by the first link plate and a second engagement by the second link plate where the engaging position is different from the first engagement are repeated aperiodically. Thereby, when the chain engages with the sprocket, at an upper position that is not affected by chordal action of a chain span, periodical chordal oscillation of a chain span can be restrained and thus, noise and oscillation performance can be further improved as compared to the periodic engagement where the entire chain pitch is constant.

#### BRIEF DESCRIPTION OF THE DRAWING

FIG. 1 is an enlarged front elevational view of two adjacent link plates in a row that forms a silent chain according to an embodiment of the present invention.

FIG. 2 is a schematic illustrating engaging state of a silent chain with a sprocket.

FIG. 3 is a graph showing interrelation between a rotational cycle of a sprocket tooth and a chain lift-up.

FIG. 4 is a graph showing the result of sound level measurement test.

#### DETAILED DESCRIPTION OF THE INVENTION

5 As shown in FIG. 1, each of link plates 2 forming a silent chain 1 includes a pair of pin apertures 21 and teeth 22. A pair of connecting pins 3 inserted in the pin apertures 21 pivotably connects adjacent link plates 2A and 2B. Each of the teeth 22 of the link plates 2 are composed of an inside flank 22a and an outside flank 22b. The inside flank 22a is formed of a curved surface, preferably a circular arc surface, and the outside flank 22b is preferably formed of a flat surface.

As shown in FIG. 1, when the chain 1 is pulled straight, the inside flank 22a of link plates 2A projects (away?) from the outside flank 22b of the link plate 2B that overlaps tooth 22 of the link plate 2A. At this time, an equality,  $0.021 \cdot P \leq \delta_{\max} \leq 0.063 \cdot p$ , is satisfied, where P is the chain pitch defined by the distance between contact points of an adjacent pair of connecting pins 3 and  $\delta_{\max}$  is the maximum projection of the inside flank 22a of the link plate 2A relative to the outside flank 22b of the adjacent link plate 2B.

Here, the maximum projection  $\delta_{\max}$  of the inside flank 22a of the link plate 2A refers to the maximum value of the projection of the inside flank 22a of the link plate 2A from the outside flank 22b of the adjacent link plate 2B (see hatching portion in FIG.1) when the chain 1 is pulled straight. Also, more preferably, an equality,  $0.035 \cdot P \leq \delta_{\max} \leq 0.063 \cdot p$  is satisfied.

Next, engagement of the above-mentioned silent chain 1 with a sprocket will be described using FIG. 2. In FIG.2, an arrow mark "a" indicates the rotational direction of a sprocket S, and an arrow mark "b" indicates the running direction of a silent chain 1. Reference numerals 2A, 2B, 2C, and 2D indicate link plates that are located in a row from the retarding side of the engagement to the leading side thereof, respectively.

At the time of initial engagement with the sprocket S, the link plate 2A is lifted upwardly through contact with sprocket tooth t at Point  $E_1$  on the addendum side of the

inside flank 22a. Thereby, a chain span or a chain chord (not shown) extending from the retarding side of the link plate 2A (on the left side of FIG.2) is lifted upwardly. The lift-up  $\Delta$  of the link plate 2A at this time is shown by the distance from the position of the initial engagement of a link plate A' that engages only an outside flank from initial to final engagement with a sprocket.

When the engagement proceeds and the link plate 2A moves to the position of the link plate 2B, the engagement point with sprocket tooth t is transferred to Point E<sub>2</sub> on the addendum side from Point E<sub>1</sub> along the inside flank 22a. The link plate 2A further moves to the positions of link plates 2C and 2D with the engagement with the sprocket tooth t maintained at Point E<sub>2</sub>. In FIG. 2, a circular arc connecting each of the engaging points E<sub>2</sub> forms an engagement pitch line n.

FIG. 3 shows the amount of a lift-up of the chain span during a rotational cycle of a sprocket tooth. In FIG. 3, a dash-and-dot line indicates the variation of the chain lift-up  $\Delta$  during rotation of one sprocket tooth in the case of a chain that engages a sprocket tooth only on the outside flanks of the link plates. A dotted line indicates the variation of the chain lift-up  $\Delta$  during rotation of one sprocket tooth in the case of a chain ( $\delta_{\max}=0.021 \cdot P$ ) that engages a sprocket tooth only on the inside flanks of the link plates. A solid line indicates the variation of the chain lift-up  $\Delta$  during rotation of one sprocket tooth in the case of a chain ( $\delta_{\max}=0.035 \cdot P$ ) that engages a sprocket tooth only on the inside flanks of the link plates. As shown by the dash-and-dot line, when a sprocket rotates one tooth thereof, or  $360^\circ/z$  (z: the number of sprocket teeth), lift-up  $\Delta$  of a chain span by the sprocket gradually grows greater with the rotational speed of the sprocket and becomes the maximum value at time T/2 (T: rotational period). The lift-up  $\Delta$  of a chain span by the sprocket gradually grows smaller with the rotational speed of a sprocket thereafter, and becomes zero at time T.

In contrast, as shown in a dotted line in FIG. 3, in the case of the chain that engages only on the inside flanks of link plates, where each link plate has a maximum projection of  $\delta_{\max}(=0.021 \cdot P)$ , when a sprocket rotates one tooth thereof, lift-up  $\Delta$  of a chain span by the sprocket hardly varies during time T from the initial engagement and

maintains the value of about 0.25. At time  $T/2$ , the dotted line generally contacts the apex of the dash-and-dot line.

As can be seen from FIG. 3, in the case where a silent chain having a chain lift-up  $\Delta$  as shown by the dash-and-dot line, engages with the sprocket, the chain is lifted up to a position upper than the range of chordal action acted by the sprocket during engagement with the chain having a chain lift-up  $\Delta$  as shown in a dotted line. Such a position is the vertex of a polygonal shaped movements of a chain, or a higher position than the vertex. Thereby, at the time of engagement with the sprocket, a chain span can be lifted up to a position where chordal action of the chain span is hardly influential. As a result, chordal action can be securely restrained and noise and oscillation performance can be improved.

As shown by the solid line of FIG. 3, in the case of a chain that engages only at the inside flanks of link plates, where each of the link plates has a maximum projection of  $\delta_{\max}(=0.035 \cdot P)$ , when a sprocket rotates one tooth thereof, lift-up  $\Delta$  of a chain span by the sprocket maintains at the considerably higher position than the dash-and-dot line and the dotted line during time  $T$  from the initial engagement. Thereby, in this case, at the time of engagement with the sprocket, the chain span may be lifted up to a position where chordal action of the chain span is more hardly influential. As a result, chordal action can be more securely restrained and noise and oscillation performance can be further improved.

FIG. 4 shows the result of a sound level measuring test of various kinds of chains. In FIG. 4, the dotted line indicates a silent chain comprised of link plates whose inside flank's maximum projection  $\delta_{\max}$  is lower than  $0.021 \cdot P$ . The dash-and-dot line indicates a silent chain comprised of link plates whose inside flank's maximum projection  $\delta_{\max}$  is equal to  $0.035 \cdot P$ . The solid line indicates a silent chain composed of link plates whose inside flank's maximum projection  $\delta_{\max}$  is equal to  $0.063 \cdot P$ . As can be seen from each of the lines in FIG. 4, in the case of  $\delta_{\max}=0.035 \cdot P$  and  $\delta_{\max}=0.063 \cdot P$ , oscillation level are decreased in the entire region of sprocket rotational speeds as compared to the case of  $\delta_{\max}<0.021 \cdot P$ . In particular, when compared at peak level, in either the case of  $\delta_{\max}=0.035 \cdot P$  or  $\delta_{\max}=0.063 \cdot P$ , peak level is securely decreased as compared to the case of  $\delta_{\max}<0.021 \cdot P$ . Additionally, in FIG. 4, the case of  $\delta_{\max}=0.021 \cdot P$  is not shown,

but it may be predicted that the peak level of the case of  $\delta_{\max}=0.021 \cdot P$  will be disposed at a position slightly lower than the peak level of the dotted line.

Therefore, when an inside flank and an outside flank of each link plate are formed in such a way that inequality,  $0.021 \cdot P \leq \delta_{\max} \leq 0.063 \cdot p$  is satisfied, more preferably,  
5  $0.035 \cdot P \leq \delta_{\max} \leq 0.063 \cdot p$  is satisfied, peak sound level of oscillation can be securely reduced.

In the above-mentioned embodiment, the maximum projections  $\delta_{\max}$  of the entire link plates comprising a silent chain are predetermined at specified values that satisfy either of the above-mentioned inequalities, but the present invention is not limited to this  
10 embodiment.

In an alternative embodiment, a projection-random silent chain may be composed by disposing a first link row formed of first link plates each having a first maximum projection  $\delta_{1\max}$  (e.g.  $\delta_{1\max}=0.035$ ) and a second link row formed of second link plates each having a second maximum projection  $\delta_{2\max}$  (e.g.  $\delta_{2\max}=0.063$ ) different from the  
15 maximum projection  $\delta_{1\max}$  randomly along the length of the chain. In this case, when the chain engages with a sprocket, a first chain lift-up  $\Delta$  by the first link plate and a second chain lift-up  $\Delta$  by the second link plate are different, and the first and second lift-up  $\Delta$  are aperiodically repeated.

Thereby, at the time of engagement with a sprocket, a periodical chordal  
20 movement of a chain span may be restrained at an upper position where chordal action is hard to affect. As a result, noise and oscillation performance may be further improved as compared to the case of engagement where a constant chain lift-up  $\Delta$  is periodically repeated.

In another embodiment, a pitch-random silent chain may be composed by  
25 disposing a first link row formed of first link plates each having a first chain pitch  $P_1$  and a second link row formed of second link plates each having a second chain pitch  $P_2$  different from the first chain pitch  $P_1$  randomly along the length of the chain. In this case, as with the previous embodiment, when a chain engages with a sprocket, an engagement by a first link plate and an engagement by a second link plate are aperiodically repeated. Thereby, at

the time of engagement with a sprocket, at an upper position where chordal action is hard to affect, noise and oscillation performance may be further improved as compared to the case of periodic engagement by the link plates each having a constant chain pitch.

5 In another alternative embodiment, a projection-random and pitch-random silent chain may be composed by combining the previous two embodiments. The projection-random portion of the silent chain may be composed by disposing a first link row formed of first link plates each having a first maximum projection  $\delta_{1\max}$  (e.g.  $\delta_{1\max}=0.035$ ) and a second link row formed of second link plates each having a second maximum projection  $\delta_{2\max}$  (e.g.  $\delta_{2\max}=0.063$ ) different from the maximum projection  $\delta_{1\max}$  randomly along  
10 the length of the chain and the pitch-random portion of the silent chain may be composed by disposing a first link row formed of first link plates each having a first chain pitch  $P_1$  and a second link row formed of second link plates each having a second chain pitch  $P_2$  different from the first chain pitch  $P_1$  randomly along the length of the chain. In this case, noise and oscillation performance may be much further improved.

15 In the above-mentioned embodiment, a silent chain of inside-flank-engagement-type from initial to final engagement was shown, but the present invention can also be applied to a silent chain that engages from an inside flank at the initial engagement and engages at an outside flank at the final engagement. Moreover, a rocker-joint-type silent chain was shown in the above-mentioned embodiment, but the present invention can also  
20 be applied to a silent chain using round pins as connecting pins.

Accordingly, it is to be understood that the embodiments of the invention herein described are merely illustrative of the application of the principles of the invention. Reference herein to details of the illustrated embodiments is not intended to limit the scope of the claims, which themselves recite those features regarded as essential to the  
25 invention.